

A brief story of numerical diffusion in SPH

Matteo Antuono & Salvatore Marrone

CNR-INM, National Research Council of Italy Institute of Marine Engineering

- SPH: Origins and early applications to fluid dynamics
- Noise in WC-SPH and motivation to the use of diffusive models
- Diffusive models in WC-SPH and inspiration from other numerical schemes
- The δ-SPH
- Further diffusive schemes in SPH
- Models stemming from the δ -SPH
- Combination of diffusion and shifting techniques
- Recent advances in the use of Riemann solvers in SPH
- Diffusion and acoustic noise: the acoustic damper

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- The δ-SPH
- Further diffusive schemes in SPH
- Models stemming from the δ-SPH
- Combination of diffusion and shifting techniques
- Recent advances in the use of Riemann solvers in SPH
- Diffusion and acoustic noise: the acoustic damper

PART I

R. A. Gingold, J. J. Monaghan, Smoothed particle hydrodynamics: theory and application to non-spherical stars, *Monthly Notices of the Royal Astronomical Society*, Volume 181, Issue 3, **December 1977**

L. B. Lucy, "A numerical approach to the testing of the fission hypothesis." *Astronomical Journal*, vol. 82, **December 1977**, p. 1013-1024. 82 (1977): 1013-1024.

R. A. Gingold, J. J. Monaghan, Smoothed particle hydrodynamics: theory and application to non-spherical stars, *Monthly Notices of the Royal Astronomical Society*, Volume 181, Issue 3, **December 1977**

L. B. Lucy, "A numerical approach to the testing of the fission hypothesis." *Astronomical Journal,* vol. 82, **December 1977**, p. 1013-1024. 82 (1977): 1013-1024.

First applications in gas dynamics and astrophysics (compressible fluids)

1D dynamics: shock tubes, Riemann problems, ...

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-	/

oscillations of the velocity field larger than those in the density/pressure field

This issue motivated the definition of bulk viscosity to reduce the oscillations in the velocity field:

J.J Monaghan, R.A Gingold, *Shock simulation by the particle method SPH*, Journal of Computational Physics, Volume 52, Issue 2, 1983, Pages 374-389,

 \Rightarrow definition of the artificial viscosity (later used as a real viscous term)

First applications to hydrodynamics (weakly-compressible fluids)

J.J. Monaghan, *Simulating Free Surface Flows with SPH*, Journal of Computational Physics, Volume 110, Issue 2, 1994, Pages 399-406 (received October 1992)

2D simulations: flows past a cylinder

Takeda, Hidenori, Shoken M. Miyama, and Minoru Sekiya. "Numerical simulation of viscous flow by smoothed particle hydrodynamics." *Progress of theoretical physics* 92.5 (1994): 939-960.

J. P. Morris, P. J. Fox, and Y. Zhu. "Modeling low Reynolds number incompressible flows using SPH." *Journal of computational physics* 136.1 (1997): 214-226. ⇒ viscosity formulation of Morris et al.(1997) First applications to hydrodynamics (weakly-compressible fluids)

J.J. Monaghan, *Simulating Free Surface Flows with SPH*, Journal of Computational Physics, Volume 110, Issue 2, 1994, Pages 399-406 (received October 1992)

	Some issues on the pressure field are pointed out:
2D simulations: flows past a cylinder	Morris et al. (1997) "The SPH dynamic pressure profile shows small local fluctuations"
Takeda, Hidenori, Shoken M. Miyama, and Minoru Sekiya. "Nume hydrodynamics." <i>Progress of theoretical physics</i> 92.5 (1994): 939	"Once again, however, small pressure fluctuations were observed near the boundary."

J. P. Morris, P. J. Fox, and Y. Zhu. "Modeling low Reynolds number incompressible flows using SPH." *Journal of computational physics* 136.1 (1997): 214-226. ⇒ viscosity formulation of Morris et al.(1997) ...but people did not like to talk about problems.....

Herant, M. "Dirty tricks for sph." *Memorie della Societa Astronomica Italiana* 65 (1994): 1013.

Probably, the bad name of SPH as a solver spread out in these years (i.e. 1992-2002)

... but people did not like to talk about problems.....

Herant, M. "Dirty tricks for sph." *Memorie della Società Astronomica Italiana* 65 (1994): 1013.

Probably, the bad name of SPH as a solver spread out in these years (i.e. 1992-2002)

In any case, different approaches were developed over the 2000's (maybe to overcome some of these issues)

Riemann solvers for particle interactions (more diffusion):

J.P. Vila, *On particle weighted methods and smooth particle hydrodynamics*, (1999), Mathematical Models and Methods in Applied Sciences 161-209

A.N. Parshikov, S.A. Medin , I.I. Loukashenko, V.A. Milekhin, Improvements in SPH method by means of interparticle contact algorithm and analysis of perforation tests at moderate projectile velocities, International Journal of Impact Engineering 24 (2000) 779-796 SPH for incompressible fluids (no acoustic noise)

S. Koshizuka, N. Atsushi, O. Yoshiaki, "Numerical analysis of breaking waves using the moving particle semi-implicit method." *International journal for numerical methods in fluids* 26.7 (1998): 751-769.

S.J. Cummins, M. Rudman. "An SPH projection method." *Journal of computational physics* 152.2 (1999): 584-607.

H. Gotoh, T. Sakai, Lagrangian Simulation of Breaking Waves Using Particle Method, Coastal Engineering Journal, vol 41, (1999) - Issue 3-4

Finally, problems came out

Imaeda, Y. & Inutsuka, S.I. Shear Flows in Smoothed Particle Hydrodynamics *The Astrophysical Journal*, **2002**, *5*69, 501

Colagrossi A. & Landrini M.,Numerical simulation of interfacial flows by smoothed particle hydrodynamics, Journal of Computational Physics 191 (**2003**) 448–475

Evolutionary calculations of rotating gaseous flows around astrophysical objects with standard smoothed particle hydrodynamics (SPH) result in inaccurate evolutions of shear flows. The **large density errors** emerge within one dynamical time of the system...

Although the gross features, e.g. the free-surface profile, of the three solutions are practically the same, it is apparent the growth of **high-frequency pressure oscillations** in solution (*A*), (...) These spurious oscillations, and their consequences, can be significantly reduced by inserting an artificial viscous term in the momentum evolution

equation, as the solution (B) shows.

R.A. Dalrymple, B.D. Rogers, Numerical modeling of water waves with the SPH method, Coastal Engineering 53 (**2006**) 141-147

(...), the application of this methodology can lead to **unphysical behaviour** at the free surface **due to** slight **density variations** being magnified by the equation of state.

Finally, problems came out

Imaeda, Y. & Inutsuka, S.I. Shear Flows in Smoothed Particle Hydrodynamics *The Astrophysical Journal*, **2002**, *5*69, 501

XSPH, artificial viscosity

Colagrossi A. & Landrini M.,Numerical simulation of interfacial flows by smoothed particle hydrodynamics, Journal of Computational Physics 191 (**2003**) 448–475

density re-initialization through MLS filter

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R.A. Dalrymple, B.D. Rogers, Numerical modeling of water waves with the SPH method, Coastal Engineering 53 (**2006**) 141-147

XSPH, Shephard filtering

(...), the application of this methodology can lead to **unphysical behaviour** at the free surface **due to** slight **density variations** being magnified by the equation of state.

$$\begin{aligned} f & \frac{\mathrm{d}\rho}{\mathrm{d}t} = -\rho \,\nabla \cdot \boldsymbol{u} \\ \rho & \frac{\mathrm{d}\boldsymbol{u}}{\mathrm{d}t} = -\nabla p + (\lambda + \mu) \nabla \left(\nabla \cdot \boldsymbol{u}\right) + \mu \,\nabla^2 \boldsymbol{u} \\ p &= f(\rho) \\ \zeta & \frac{\mathrm{d}}{\mathrm{d}t} = \frac{\partial}{\partial t} + \boldsymbol{u} \cdot \nabla \end{aligned}$$

The fluid is assumed to be:

- compressible
- barotropic (density and pressure related through a state equation)

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To approximate incompressible fluids, we require the fluid to be **weakly-compressible**

$$\frac{\mathrm{d}p}{\mathrm{d}\rho} \,=\, c^2(\rho) \,\gg\, U_0^2$$

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$$\frac{\mathrm{d}p}{\mathrm{d}\rho} \,=\, c^2(\rho) \,\gg\, U_0^2$$

$$\begin{aligned} \int \frac{\mathrm{d}\rho_i}{\mathrm{d}t} &= -\rho_i \, \langle \nabla \cdot \boldsymbol{u} \rangle_i \\ \rho_i \frac{\mathrm{d}\boldsymbol{u}_i}{\mathrm{d}t} &= -\langle \nabla p \rangle_i \, + \, \langle \nabla \cdot \nabla \rangle_i \\ p_i &= f(\rho_i) \\ \int \frac{\mathrm{d}\boldsymbol{x}_i}{\mathrm{d}t} &= \boldsymbol{u}_i \end{aligned}$$

- The fluid domain is discretized in a set of moving particles
- the differential operators are replaced by their smoothed counterparts

$$\begin{cases} \frac{\mathrm{d}\rho_i}{\mathrm{d}t} = -\rho_i \langle \nabla \cdot \boldsymbol{u} \rangle_i \\\\ \rho_i \frac{\mathrm{d}\boldsymbol{u}_i}{\mathrm{d}t} = -\langle \nabla p \rangle_i + \langle \nabla \cdot \nabla \rangle_i \\\\ p_i = f(\rho_i) \\\\ \frac{\mathrm{d}\boldsymbol{x}_i}{\mathrm{d}t} = \boldsymbol{u}_i \end{cases}$$

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Noise in WC-SPH and motivation to the use of diffusive models



Noise in WC-SPH and motivation to the use of diffusive models



Wedge entry problem with a deadrise angle of 15° (freely dropped from height h=0.75 m). Pressure solution at time t = 0.008s using the δ^+-SPH

Noise in WC-SPH and motivation to the use of diffusive models

example of high-frequency noise: inviscid oscillating drop in a central force field







central force field with potential: $\varphi = -B^2 (x^2 + y^2)$



$$\begin{aligned} \int \frac{\mathrm{d}\rho_i}{\mathrm{d}t} &= -\rho_i \, \langle \nabla \cdot \boldsymbol{u} \rangle_i \\ \rho_i \frac{\mathrm{d}\boldsymbol{u}_i}{\mathrm{d}t} &= -\langle \nabla p \rangle_i + \langle \nabla \cdot \nabla \rangle_i \\ p_i &= f(\rho_i) \\ \frac{\mathrm{d}\boldsymbol{x}_i}{\mathrm{d}t} &= \boldsymbol{u}_i \end{aligned}$$

- Why the pressure field is more noisy than the velocity one?
- How is possible to regularize the pressure field (at least for high-frequency noise)?

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DIFFUSIVE TERM

- Why the pressure field is more noisy than the velocity one?
- How is possible to regularize the pressure field (at least for high-frequency noise)?

The diffusive term in the continuity equation helps removing the high-frequency noise in the density/pressure fields (similarly to what the viscous term does in the momentum equation)

In the SPH literature the diffusion in the continuity equation has been first proposed in....

D. Molteni, A. Colagrossi, A simple procedure to improve the pressure evaluation in hydrodynamic context using the SPH, Computer Physics Communications, Volume 180, Issue 6, **2009**, Pages 861-872, Received 14 February 2008, Accepted 2 December 2008

A. Ferrari, M. Dumbser, E. F. Toro, A. Armanini, A new 3D parallel SPH scheme for free surface flows, Computers & Fluids, Volume 38, Issue 6, **2009**, Pages 1203-1217, Received 30 July 2008, Accepted 19 November 2008

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"Such a procedure is based on the use of a density diffusion term in the equation for the mass conservation"

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Riemann solvers in SPH

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"The new key idea consists of introducing a monotone upwind flux, following directly the Ben Moussa and Vila approach, but only for the density equation" In the SPH literature the diffusion in the continuity equation has been first proposed in....

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Riemann solvers in SPH

 N
\longrightarrow
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"The new key idea consists of introducing a monotone upwind flux, following directly the Ben Moussa and Vila approach, but only for the density equation" Similar ideas have been proposed in....

Magneto-hydrodynamics (similarities between the magnetic and density field equations with diffusion)

A. Dedner, F. Kemm, D. Kroner, C.D. Munz, T. Schnitzer, M. Wesenberg, *Hyperbolic Divergence Cleaning for the MHD Equations*, Journal of Computational Physics 175, 645–673 (2002)

Thermodynamics

J. R. Clausen,

Entropically damped form of artificial compressibility for explicit simulation of incompressible flow, PHYSICAL REVIEW E 87, 013309 (**2013**)

The temperature fluctuations are related to the density field to minimize acoustic components

Molteni & Colagrossi (2009) // Ferrari et al. (2009)

$$\mathcal{D}_i \simeq \xi h c_0 \Delta \rho$$

- *h* smoothing length (i.e. reference length)
- c_o reference sound speed
- ξ dimensionless parameter

$$\begin{cases} \frac{\mathrm{d}\rho_i}{\mathrm{d}t} = -\rho_i \langle \nabla \cdot \boldsymbol{u} \rangle_i + \mathcal{D}_i \\\\ \rho_i \frac{\mathrm{d}\boldsymbol{u}_i}{\mathrm{d}t} = -\langle \nabla p \rangle_i + \langle \nabla \cdot \mathbb{V} \rangle_i \\\\ p_i = f(\rho_i) \\\\ \frac{\mathrm{d}\boldsymbol{x}_i}{\mathrm{d}t} = \boldsymbol{u}_i \end{cases}$$

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- ξ dimensionless parameter





Hydrostatic solution. Left panels: SPH with the diffusive term of Ferrari et al. [11].

Antuono et al. (2012)

$$\mathcal{D}_i \simeq \delta h^3 c_0 \Delta^2 \rho$$

- *h* smoothing length (i.e. reference length)
- c_o reference sound speed
- δ dimensionless parameter



 $\begin{cases} \frac{\mathrm{d}\rho_i}{\mathrm{d}t} = -\rho_i \langle \nabla \cdot \boldsymbol{u} \rangle_i + \mathcal{D}_i \\\\ \rho_i \frac{\mathrm{d}\boldsymbol{u}_i}{\mathrm{d}t} = -\langle \nabla p \rangle_i + \langle \nabla \cdot \nabla \rangle_i \\\\ p_i = f(\rho_i) \\\\ \frac{\mathrm{d}\boldsymbol{x}_i}{\mathrm{d}t} = \boldsymbol{u}_i \end{cases}$

Consistent close to the free-surface

Hydrostatic solution. Left panels: SPH with the diffusive term of Ferrari et al. [11]. Right panels: SPH with the diffusive term of Antuono et al. [13].

$$\begin{cases} \frac{\mathrm{d}\rho_i}{\mathrm{d}t} = -\rho_i \langle \nabla \cdot \boldsymbol{u} \rangle_i + \mathcal{D}_i \\\\ \rho_i \frac{\mathrm{d}\boldsymbol{u}_i}{\mathrm{d}t} = -\langle \nabla p \rangle_i + \langle \nabla \cdot \mathbf{V} \rangle_i \\\\ p_i = f(\rho_i) \\\\ \frac{\mathrm{d}\boldsymbol{x}_i}{\mathrm{d}t} = \boldsymbol{u}_i \end{cases}$$

$$\mathcal{D}_{i} = \delta h c_{0} \left[2 \sum_{j} \psi_{ji} \frac{(\boldsymbol{r}_{j} - \boldsymbol{r}_{i}) \cdot \nabla_{i} W_{ji}}{\|\boldsymbol{r}_{j} - \boldsymbol{r}_{i}\|^{2}} V_{j} \right]$$
$$\psi_{ji} = \left[(\rho_{j} - \rho_{i}) - \frac{1}{2} \left(\langle \nabla \rho \rangle_{j}^{L} + \langle \nabla \rho \rangle_{i}^{L} \right) \cdot (\boldsymbol{r}_{j} - \boldsymbol{r}_{i}) \right]$$
renormalized density gradient

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P.W. Randles, L.D. Libersky, *Smoothed particle hydrodynamics: some recent improvements and applications*, Comput. Methods Appl. Mech. Engrg. 139 (1996) 375–408

The δ -SPH preserves the mass of the fluid bulk and satisfies the conservation of both linear and angular momenta

The optimal choice is $\delta \approx 0.1-0.2$ [through a linear stability analysis performed in Antuono et al. (2012)]

M. D. Green, R. Vacondio, J. Peiró, A smoothed particle hydrodynamics numerical scheme with a consistent diffusion term for the continuity equation, Computers and Fluids 179 (2019) 632–644

"We propose to re-interpret the formulation of Antuono et al. (2012) as an approximate Riemann solver with first-order reconstruction of the density at the particle-particle interface."

$$\mathcal{D}_i = \delta h c_0 \left[2 \sum_j \psi_{ji} rac{(oldsymbol{r}_j - oldsymbol{r}_i) \cdot
abla_i W_{ji}}{\|oldsymbol{r}_j - oldsymbol{r}_i\|^2} V_j
ight]$$

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Time integration

Some good ideas from Finite Volume schemes: **FROZEN DIFFUSION**

A. Jamenson, W. Schmidth, E. Turkel, *Numerical solution of the Euler equations by finite volume methods using Runge-Kutta time-stepping schemes*, in: AIAA 14th Fluid and Plasma Dynamics Conference, Palo Alto, CA, June 23–25, 1981.

 $\frac{d\boldsymbol{w}}{dt} = \boldsymbol{Q} + \boldsymbol{D}$ numerical diffusion

standard SPH terms

Time integration

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 $\frac{d \boldsymbol{w}}{d t} = \boldsymbol{Q} + \boldsymbol{D}$ numerical diffusion

standard SPH terms

fourth-order Runge-Kutta scheme with Frozen Diffusion

$$w^{(0)} = w^{n}$$

$$w^{(1)} = w^{(0)} + Q(w^{(0)}) \Delta t/2 + D(w^{(0)}) \Delta t/2$$

$$w^{(2)} = w^{(0)} + Q(w^{(1)}) \Delta t/2 + D(w^{(0)}) \Delta t/2$$

$$w^{(3)} = w^{(0)} + Q(w^{(2)}) \Delta t + D(w^{(0)}) \Delta t$$

$$w^{(4)} = w^{(0)} + [Q(w^{(0)}) + 2Q(w^{(1)}) + 2Q(w^{(2)}) + Q(w^{(3)})] \Delta t/6 + D(w^{(0)}) \Delta t$$

$$w^{n+1} = w^{(4)}.$$

Time integration

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$\frac{d\boldsymbol{w}}{dt} = \boldsymbol{Q} + \boldsymbol{D}$ numerical diffusion

standard SPH terms

fourth-order Runge-Kutta scheme with Frozen Diffusion

$$\begin{split} \boldsymbol{w}^{(0)} &= \boldsymbol{w}^{n} \\ \boldsymbol{w}^{(1)} &= \boldsymbol{w}^{(0)} + \boldsymbol{Q}(\boldsymbol{w}^{(0)}) \,\Delta t/2 + \boldsymbol{D}(\boldsymbol{w}^{(0)}) \,\Delta t/2 \\ \boldsymbol{w}^{(2)} &= \boldsymbol{w}^{(0)} + \boldsymbol{Q}(\boldsymbol{w}^{(1)}) \,\Delta t/2 + \boldsymbol{D}(\boldsymbol{w}^{(0)}) \,\Delta t/2 \\ \boldsymbol{w}^{(3)} &= \boldsymbol{w}^{(0)} + \boldsymbol{Q}(\boldsymbol{w}^{(2)}) \,\Delta t + \boldsymbol{D}(\boldsymbol{w}^{(0)}) \,\Delta t \\ \boldsymbol{w}^{(4)} &= \boldsymbol{w}^{(0)} + \left[\boldsymbol{Q}(\boldsymbol{w}^{(0)}) + 2 \,\boldsymbol{Q}(\boldsymbol{w}^{(1)}) + 2 \,\boldsymbol{Q}(\boldsymbol{w}^{(2)}) + \boldsymbol{Q}(\boldsymbol{w}^{(3)}) \right] \Delta t/6 + \boldsymbol{D}(\boldsymbol{w}^{(0)}) \,\Delta t \\ \boldsymbol{w}^{n+1} &= \boldsymbol{w}^{(4)} \,. \end{split}$$

Time integration

a further constraint to the time step has to be added because of the presence of diffusion in the continuity equation

$$\Delta t_c = K_c \left(\frac{h}{c_0}\right) \qquad K_c = 1.3$$
 with C2 Wendland kernel

$$\Delta t_{\nu} = \frac{1}{\alpha} \left(\frac{h}{c_0} \right)$$

$$\Delta t_a = 0.25 \min_i \sqrt{\frac{h}{\|\boldsymbol{a}_i\|}}$$

$$\Delta t_{\delta} = \frac{0.44}{\delta} \left(\frac{h}{c_0} \right)$$

$$\Delta t = \min(\Delta t_{\nu}, \Delta t_{a}, \Delta t_{\delta}, \Delta t_{c})$$

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$$\Delta t_{\delta} = \frac{0.44}{\delta} \left(\frac{h}{c_0} \right)$$

For δ ~0.1-0.2 this is NOT the most restrictive bound

$$\Delta t = \min(\Delta t_{\nu}, \Delta t_{a}, \Delta t_{\delta}, \Delta t_{c})$$

Further diffusive schemes in SPH

R. Fatehi and M. T. Manzari, *A consistent and fast weakly compressible smoothed particle hydrodynamics with a new wall boundary condition*, Int. J. Numer. Meth. Fluids 2012; 68:905-921

Diffusion in the continuity equation as consequence of the use of different time-integration schemes in the continuity and momentum equations => the coefficient depends on the CFL

P. Ramachandran, K. Puri, *Entropically damped artificial compressibility for SPH*, Computers and Fluids 179 (2019) 579-594

Diffusion in the equation of the pressure field (in place of the density field) following the theoretical work of Clausen (2013)

G. Fourtakas, J.M. Dominguez, R. Vacondio, B.D. Rogers (2019) *Local uniform stencil (LUST) boundary condition for arbitrary 3-D boundaries in parallel smoothed particle hydrodynamics (SPH) models*. Comput Fluids 190:346-361.

Diffusion term as in Molteni & Colagrossi (2009) applied to the dynamic component of the density field (the hydrostatic component is removed)

J.J. De Courcy, T.C.S. Rendall, L. Constantin, B. Titurus, J.E. Cooper, *Incompressible* δ -SPH via artificial compressibility, Computer Methods in Applied Mechanics and Engineering 420 (2024) 116700

Diffusion in the continuity equation is obtained by using artificial compressibility => close analogies with the δ -SPH scheme

δ-SPH

δplus -SPH

+ shifting techniques

P.N. Sun, A. Colagrossi, S. Marrone, A.M. Zhang, *The δplus-SPH model: Simple procedures for a further improvement of the SPH scheme*, Comput. Methods Appl. Mech. Engrg. 315 (2017) 25-49.

δ -ALE-SPH

Arbitrary-Lagrangian
 -Eulerian framework
 M. Antuono a , P.N. Sun, S. Marrone, A. Colagrossi, The δ-ALE-SPH model: An arbitrary
 Lagrangian-Eulerian framework for the δ-SPH model with particle shifting technique, Computers and Fluids 216 (2021) 104806

δLES-SPH

 Large-Eddy-Simulation framework
 M Antuono, S Marrone, A Di Mascio, A Colagrossi, Smoothed particle hydrodynamics method from a large eddy simulation perspective. Generalization to a quasi-Lagrangian model, Physics of Fluids Volume 33 Numero 1 (2021)

A brief story of numerical diffusion in SPH

PART II

- SPH: Origins and early applications to fluid dynamics
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- Diffusion and acoustic noise: the acoustic damper

$\delta\mbox{-SPH}$ has been applied in several contexts with great success



1.5 г 1.5 y/H SPH H/∆x = 400 LS-FVM Re = 5000 y/H P/pgH H/Ax = 400 1 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1 t(g/H) =2.0 0.5 0.5 1.5 y/H LS-FVM H/∆x = 400 SPH t(g/H)⁶=5.81 y/H $H/\Delta x = 400$ 0.5 0.5 x/H у/Н Г 1.5 y/H SPH LS-FVM H/∆x = 400 t(g/H)⁵=6.41 $H/\Delta x = 400$ 0.5 x/H y/H 1.5 г LS-FVM SPH t(g/H)⁵=6.80 y/H $H/\Delta x = 400$ $H/\Delta x = 400$ 0.5 0.5 5 x/H 3 x/H

Dam-break flow

Weakly-Compressible δ -SPH

Incompressible FVM

...and the $\delta\text{-SPH}$ paradigm was extended to several other contexts

Multi-phase flows



Large-Eddy Simulation models



Hammani, I., et al. "Detailed study on the extension of the δ -SPH model to multi-phase flow." CMAME 368 (2020): 113189.

Di Mascio, A., et al. "Smoothed particle hydrodynamics method from a large eddy simulation perspective." *Physics of Fluids* 29.3 (2017).

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Large-Eddy Simulation models



Di Mascio, A., et al. "Smoothed particle hydrodynamics method from a large eddy simulation perspective." *Physics of Fluids* 29.3 (2017).

Formulation in a quasi-lagrangian framework

Diffusive terms, however, are not a panacea...





Alongside the diffusive terms, a cure for particle positions: the $\delta^{\text{+}}\text{-}\text{SPH}$

 δ^+ -SPH: correction of particle advection following Lind et al. 2012

$$\begin{cases} \boldsymbol{r}_i^* = \boldsymbol{r}_i + \delta \boldsymbol{r}_i \\ \delta \boldsymbol{r}_i := -\text{CFL} \cdot \text{Ma} \cdot (2h_{ij})^2 \cdot \sum_j \left[1 + R \left(\frac{W_{ij}}{W(\Delta x_i)} \right)^n \right] \nabla_i W_{ij} \varphi_{ij} \frac{m_j}{(\rho_i + \rho_j)} \end{cases}$$

correction for the free-surface

$$\hat{\delta r_i} = \begin{cases} 0 & \text{if } \lambda_i < 0.4 \text{ and } i \in \text{free-surface region} \\ (\mathbb{I} - \mathbf{n}_i \otimes \mathbf{n}_i) \, \delta \mathbf{r}_i & \text{if } \lambda_i \ge 0.4 \text{ and } i \in \text{free-surface region} \\ \delta \mathbf{r}_i & i \notin \text{free-surface region} \end{cases}$$

LIND, S.J. et al. "Incompressible smoothed particle hydrodynamics for free-surface flows: A generalised diffusion-based algorithm for stability and validations for impulsive flows and propagating waves" JCP (2012)

SUN, P. N., et al. "The δ^+ -SPH model: Simple procedures for a further improvement of the SPH scheme" CMAME, 2017.



In some cases it can result in a substantial improvement



In some cases it can result in a substantial improvement

COLAGROSSI, A., et al. Viscous flow past a cylinder close to a free surface: Benchmarks with steady, periodic and metastable responses, solved by meshfree and mesh-based schemes. Computers & Fluids, 2019.

Lagrangian derivative must be re-defined for a particle moving with advection velocity $(\vec{u} + \delta \vec{u})$

 $\frac{\mathrm{d}f}{\mathrm{d}t} := \frac{\partial f}{\partial t} + \nabla f \cdot (\vec{u} + \delta \vec{u})$

Thus leading to the δ -ALE-SPH scheme

$$\begin{aligned} \frac{\mathrm{d}\rho}{\mathrm{d}t} &= -\rho \operatorname{div}(\vec{u} + \delta \vec{u}) + \operatorname{div}(\rho \,\delta \vec{u}) + \mathcal{D}^{\rho} \,, \\ \frac{\mathrm{d}m}{\mathrm{d}t} &= m \, \frac{\mathrm{div}(\rho \,\delta \vec{u})}{\rho} + \mathcal{D}^{m} \,, \\ \frac{\mathrm{d}(m\vec{u})}{\mathrm{d}t} &= m \left[-\frac{\nabla p}{\rho} + \frac{\mathrm{div}(\mathbb{T}^{\nu})}{\rho} + \vec{g} + \frac{\mathrm{div}(\rho \,\vec{u} \otimes \delta \vec{u})}{\rho} \right] \,, \\ \frac{\mathrm{d}\vec{r}}{\mathrm{d}t} &= \vec{u} + \delta \vec{u} \,, \quad V = m \, \big/ \rho \,, \quad p = c_0^2 \, (\rho - \rho_0) \,. \end{aligned}$$

Lagrangian derivative must be re-defined for a particle moving with advection velocity $(\vec{u} + \delta \vec{u})$

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Lagrangian derivative must be re-defined for a particle moving with advection velocity $(\vec{u} + \delta \vec{u})$

 $\frac{\mathrm{d}f}{\mathrm{d}t} := \frac{\partial f}{\partial t} + \nabla f \cdot (\vec{u} + \delta \vec{u})$

$$|\delta m{u}| \ll |m{u}|$$

neglecting mass exchanges : Quasi-Lagrangian scheme with constant masses

$$\begin{cases} \frac{\mathrm{d}\rho_i}{\mathrm{d}t} = -\rho_i \langle \operatorname{div}(\vec{u} + \delta \vec{u}) \rangle_i + \langle \operatorname{div}(\rho \delta \vec{u}) \rangle_i + \mathcal{D}_i^{\rho} \\ \frac{\mathrm{d}\vec{u}_i}{\mathrm{d}t} = -\frac{\langle \nabla p \rangle_i}{\rho_i} + \frac{\langle \operatorname{div}(\mathbb{T}^{\nu}) \rangle_i}{\rho_i} + \vec{g} + \langle \operatorname{div}(\vec{u} \otimes \delta \vec{u}) \rangle_i - \vec{u}_i \langle \operatorname{div}(\delta \vec{u}) \rangle_i \\ \frac{\mathrm{d}\vec{r}_i}{\mathrm{d}t} = \vec{u}_i + \delta \vec{u}_i, \quad V_i(t) = m_{0i} / \rho_i(t), \quad p = c_0^2 \left(\rho - \rho_0\right). \end{cases}$$

ANTUONO, M., et al. The δ-ALE-SPH model: An arbitrary Lagrangian-Eulerian framework for the δ-SPH model with particle shifting technique. C&F, 2021

Taylor-Green vortex flow



Pressure history measured in the center



Pressure profile $2.5 [p/p(t_0)]$ δ-ALE-SPH P/P Re=1000, tU/L=6.00, - δ^+ -SPH (Sun et al. 2017) 3 Re = 1000Section y=0.5L – δ-SPH 1.5 L/∆x =400 - Analytical Solution 2 0.5 0 δ-ALE-SPH 0.2 0.4 0.6 0.8 x/L δ^+ -SPH (Sun et al. 2017) δ-SPH **Analytical Solution** 8 tU/L 10 2 6

Pressure history measured in the center

All these enhancements bring clear benefits to practical simulations

Extreme vertical sloshing in an aircraft wing tank

Flow is accelerated up to ~10g and the tank oscillates at a frequency of 6.5 Hz



t = 0.108 s

t = 1.270 s





Applications to complex problems

All these enhancements bring clear benefits to practical simulations



All these enhancements bring clear benefits to practical simulations

In order to accurately reproduce this phenomenon we need:

- Pressure fields free from numerical noise
- Accurate vorticity fields and low numerical diffusion
- Turbulence modelling

- \rightarrow Diffusive terms
- \rightarrow Quasi-Lagrangian scheme
- \rightarrow LES model



MICHEL, J., et al. "Energy dissipation in violent three-dimensional sloshing flows induced by high-frequency vertical accelerations". PoF, 2022.

Primitive Variable Riemann Solver (PVRS) in place of δ -SPH diffusive terms

$$\begin{cases} \frac{d\rho_i}{dt} = -\rho_i \operatorname{div}(\boldsymbol{u}_i + \boldsymbol{\delta}\boldsymbol{u}_i) + \operatorname{div}(\rho_i \boldsymbol{\delta}\boldsymbol{u}_i) + \Theta_{i,Rie}^{\rho} \\ \rho_i \frac{d\boldsymbol{u}_i}{dt} = \boldsymbol{F}_i^{\rho} + \boldsymbol{F}_i^{\mu} + \boldsymbol{f}_i + \operatorname{div}(\rho_i \boldsymbol{u}_i \otimes \boldsymbol{\delta}\boldsymbol{u}_i) + \Theta_{i,Rie}^{\boldsymbol{u}} \\ \frac{d\boldsymbol{x}_i}{dt} = \boldsymbol{u}_i + \boldsymbol{\delta}\boldsymbol{u}_i, \quad V_i(t) = m_i/\rho_i(t), \quad P_i = c_0^2(\rho_i - \rho_0) \end{cases}$$

$$\Theta_{i,Rie}^{\rho} = -\rho_i \sum_i (2\boldsymbol{u}_E - (\boldsymbol{u}_i + \boldsymbol{u}_j)) \cdot \boldsymbol{\nabla}_i W_{ij} V_j$$
$$\Theta_{i,Rie}^{\boldsymbol{u}} = -\sum_i [2P_E - (P_i + P_j)] \boldsymbol{\nabla}_i W_{ij} V_j$$

where u_E and P_E are the solutions of the Riemann problem

A.N. Parshikov, Application of a solution to the Riemann problem in the SPH method, Comput. Math. Math. Phys. 1999.

Primitive Variable Riemann Solver (PVRS) in place of δ -SPH diffusive terms

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It can be shown that:

$$\Theta_{i,Rie}^{\rho} = -\frac{3 R^2}{8} \alpha \Delta (\nabla \cdot \boldsymbol{u}) + \frac{1}{c_0 \rho_0} \frac{R^3}{16} \beta \Delta^2 P + \mathcal{O}(R^4)$$
$$\Theta_{i,Rie}^{\boldsymbol{u}} = +\frac{3}{8} R^2 \alpha \nabla (\Delta P) - \rho_0 c_0 \frac{R^3}{120} \gamma \left[\Delta^2 \boldsymbol{u} + 4 \nabla (\Delta (\nabla \cdot \boldsymbol{u})) \right] + \mathcal{O}(R^4)$$

Primitive Variable Riemann Solver (PVRS) in place of δ -SPH diffusive terms

$$\begin{aligned} \frac{d\rho_i}{dt} &= -\rho_i \operatorname{div}(\boldsymbol{u}_i + \boldsymbol{\delta}\boldsymbol{u}_i) + \operatorname{div}(\rho_i \boldsymbol{\delta}\boldsymbol{u}_i) + \boldsymbol{\Theta}_{i,Rie}^{\rho} \\ \rho_i \frac{d\boldsymbol{u}_i}{dt} &= \boldsymbol{F}_i^{\rho} + \boldsymbol{F}_i^{\mu} + \boldsymbol{f}_i + \operatorname{div}(\rho_i \boldsymbol{u}_i \otimes \boldsymbol{\delta}\boldsymbol{u}_i) + \boldsymbol{\Theta}_{i,Rie}^{\boldsymbol{u}} \\ \frac{d\boldsymbol{x}_i}{dt} &= \boldsymbol{u}_i + \boldsymbol{\delta}\boldsymbol{u}_i, \quad V_i(t) = m_i/\rho_i(t), \quad P_i = c_0^2(\rho_i - \rho_0) \end{aligned}$$

It can be shown that:

$$\Theta_{i,Rie}^{\rho} = -\frac{3}{8} \frac{R^2}{8} \alpha \Delta (\nabla \cdot \boldsymbol{u}) + \frac{1}{c_0 \rho_0} \frac{R^3}{16} \left(\Delta^2 P + \mathcal{O} \left(R^4 \right) \right)^{\text{bi-laplacian as in \delta-SPH!}} (\text{see also Green et al. 2019})$$
$$\Theta_{i,Rie}^{\boldsymbol{u}} = +\frac{3}{8} R^2 \alpha \nabla (\Delta P) - \rho_0 c_0 \frac{R^3}{120} \gamma \left[\Delta^2 \boldsymbol{u} + 4 \nabla (\Delta (\nabla \cdot \boldsymbol{u})) \right] + \mathcal{O} \left(R^4 \right)$$

Primitive Variable Riemann Solver (PVRS) in place of δ -SPH diffusive terms

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It can be shown that:

$$\Theta_{i,Rie}^{\rho} = -\frac{3}{8} \frac{R^2}{8} \alpha \Delta (\nabla \cdot \boldsymbol{u}) + \frac{1}{c_0 \rho_0} \frac{R^3}{16} \beta \Delta^2 P + \mathcal{O}(R^4) \qquad \text{diffusive term in momentum eq. is of higher order than artificial viscosity}$$
$$\Theta_{i,Rie}^{\boldsymbol{u}} = +\frac{3}{8} \frac{R^2}{8} \alpha \nabla (\Delta P) - \rho_0 \left(\frac{R^3}{120} \gamma \left[\Delta^2 \boldsymbol{u} + 4 \nabla (\Delta (\nabla \cdot \boldsymbol{u})) \right] + \mathcal{O}(R^4)$$

(a) Pressure field compared to analytic solution Observed convergence order between 2 and 3! $\frac{L}{\Delta x} = 800$ $\frac{tU}{L} = 5$ y/L $\frac{\mathcal{E}_k}{\mathcal{F}^0}$ 10 $\rho_0 U^2 / 2$ 10^{-2} 0.6 2.60.5 0.2 2.5-0.2 10^{-3} -0.6 -1 10^{-4} 100200400 L/800 Δx 0 $\cdot x/L$ 0.5 0

MICHEL, J., et al. "A regularized high-order diffusive smoothed particle hydrodynamics scheme without tensile instability" Physics of Fluids, 2023.

Acoustic waves sometimes are un unwanted noise on the solution



Acoustic waves can be un unwanted noise on the solution



Acoustic waves can be un unwanted noise on the solution



The δ^+ -SPH with the acoustic damper term

$$\begin{cases} \frac{\mathrm{d}\rho_{i}}{\mathrm{d}t} &= -\rho_{i}\sum_{j}\left(\boldsymbol{u}_{ji} + \delta\boldsymbol{u}_{ji}\right)\cdot\nabla_{i}W_{ij}V_{j} \\ &+ \sum_{j}\left(\rho_{j}\,\delta\boldsymbol{u}_{j} + \rho_{i}\,\delta\boldsymbol{u}_{i}\right)\cdot\nabla_{i}W_{ij}V_{j} + \mathcal{D}_{i}^{\rho} \\ \rho_{i}\frac{\mathrm{d}\boldsymbol{u}_{i}}{\mathrm{d}t} &= \boldsymbol{F}_{i}^{p} + \boldsymbol{F}_{i}^{v} + \boldsymbol{F}_{i}^{ad} + \rho_{i}\boldsymbol{g} \\ &+ \sum_{j}\left(\rho_{j}\,\boldsymbol{u}_{j}\otimes\delta\boldsymbol{u}_{j} + \rho_{i}\,\boldsymbol{u}_{i}\otimes\delta\boldsymbol{u}_{i}\right)\cdot\nabla_{i}W_{ij}V_{j} \\ \frac{\mathrm{d}\boldsymbol{r}_{i}}{\mathrm{d}t} &= \boldsymbol{u}_{i} + \delta\boldsymbol{u}_{i}, \quad V_{i} = m_{i}/\rho_{i}, \quad p = c_{0}^{2}(\rho - \rho_{0}), \end{cases}$$

The $\delta^{\scriptscriptstyle +}\text{-SPH}$ with the acoustic damper term

$$\boldsymbol{F}_{i}^{ad} = \alpha_{2} \rho_{0} c_{0} h \sum_{j} \left(\dot{c}_{j} + \dot{c}_{i} \right) \nabla_{i} W_{ij} V_{j} \simeq \xi \nabla \left(\nabla \cdot \boldsymbol{u} \right)$$

$$\dot{c}_k = -\dot{
ho_k}/
ho_k = \sum_l oldsymbol{u}_{lk} \cdot
abla_k W_{kl} V_l \qquad \simeq
abla \cdot oldsymbol{u}$$

 $\xi = \, lpha_2 \,
ho_0 \, c_0 \, h \,$ is a free bulk coefficient where ${\it a}_{_2}$ is a dimensionless coefficient

Similar to the artificial viscosity of Monaghan & Gingold, ξ decreases as h goes to zero

SUN, P. N., et al. Inclusion of an acoustic damper term in weakly-compressible SPH models. JCP, 2023.

Dam-break flow against a rectangular obstacle



- Particle methods, such as SPH, are more prone to particle-scale noise with respect grid-based schemes because of additional degrees of freedom
- Diffusive terms are a straightforward way to alleviate this issue
- One can follow different paths to derive diffusive terms in the continuity equations, some of those are not merely numerical expedients but rely on physical bases (e.g. δ-LES)
- They are even more effective in combination with particle shifting techniques (Quasi-Lagrangian) as the latter acts on the source of the particle-scale noise
- Specific diffusive terms can be also conceived to address acoustic noise stemming from the weak-compressibility assumption
- All these ingredients allow for tackling complex and challenging problems and ongoing research continuously increases the capabilities of the SPH scheme